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AIR-LAUNCHED MISSILE FAILURE/DAMAGE STUDY

C /F / Jawor charics Division Systems Development Department

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Naval Weapons Center China Lake, California 93555

Technical memo, Jun-Dec 76,

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### FOREWORD

This report contains the results of a study of missile structural failure/damage data. This study was made to identify major problem areas and common causes of failure/damage to airborne missiles which should be avoided in future missile design and Fleet deployment. Funding for this study was provided by the Naval Air Systems Command under Air Task AO3W-O3P2/008B/6F32.300-000.

The work presented in this report was conducted during the period of June 1976 through December 1976.

The primary sources of failure/damage data were the Fleet Support Branch of the Fleet Engineering Division at NWC and the Fleet Analysis Center, NWS, Corona Annex.

This report is released at the working level for information purposes only.

Ray W. Van Aken, Head Aeromechanics Division Systems Development Department 15 February 1977

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### SUMMARY

A study of structural failure/damage data, from various sources, such as inspection reports, fleet unsatisfactory reports and accident/incident reports, for air launched missiles was performed to determine major problem areas and common causes for the failure/damage. Missiles for which failure/damage data were studied are: SIDEWINDER (AIM-9), SPARROW (AIM-7), SHRIKE (ACM-45), BULLPUP (AIM-12), PHOENIX (AIM-54), STANDARD ARM (RIM-66, -67) and WALLEYE (AGM-62). The most common causes of structural failure/damage were found to be careless and negligent handling, and captive flight environment overstress caused by excessive motion at moveable control surfaces. Corrosion due to inadequate packaging and storage conditions was also a common cause of damage. Recommendations for investigation and study of these causes of failure/damage are made.

### INTRODUCTION

This report contains the results of a study of missile structural failure/damage data, made in order to identify major problem areas and common causes of failure/damage that should be avoided in future missile design and fleet deployment.

Although data on failures/damage was readily available, the type or format of the data was varied and was the limiting factor in the study. The first portion of the study is based on data gathered at NWC and Pt. Mugu from data files of personnel involved in the fleet support effort of the various missiles. This data varied from summaries of failure damage to informal notes (reference 1-18). Data from these sources was adequate to provide a basis for categorizing failure/damage by common cause of failure, but quantitative data was lacking since there was no means of correlating number of failures and missiles from the varied data. The major problem encountered with gathering data was that there is no control point (such as the library) where reports such as references 10 and 11 can be found, these reports are disseminated to individuals, and were kept in their files at their discretion.

The second portion of the study is based on data received from the Fleet Analysis Center (FLTAC) N.W.S., Corona Annex. Although all data

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on fleet missile problems is collected at FLTAC, it is put into coded computer data banks, and requires programming a computer code to retrieve any particular type of data such as structural failure/damage.

The data from FLTAC provided numerical data based on number of inspections reported via the Shore Maintenance Data Collection System (SMDCS).

### DISCUSSION

Data on structural failures and physical damage to missiles compiled from various sources are listed by missile in Table I. To facilitate further analysis of the failure/damage data, categorization by source or cause of failure/damage was necessary. Table II shows the data from Table I listed under four categories of cause of failure/damage. The four categories for cause of failure/damage chosen were: 1. Corrosion, 2. Handling, 3. Quality Control/Assurance, and 4. Captive Flight Environment. Although design deficiency may be a cause in some failures, it was not listed as a separate category, since it may be a factor in each of the four categories chosen. There may also be some overlap in the cause of the failures listed, as for instance; undetected damage during handling or storage may cause a failure during captive flight.

Each of the four categories can be broken down further as follows:

CORROSION: Due to packaging, storage conditions, or inadequate design (improper materials, lack of corrosion protection, etc.)

HANDLING: Improper procedures, personnel error, or inadequate design for handling.

QUALITY CONTROL/ASSURANCE: Manufacturing, inspection or design deficiency (excessive tolerances, inadequate or improper specification of heat treatment, etc.)

CAPTIVE FLIGHT LNVIRONMENT: Overstress, weather, or design deficiency.

Table III is a summary of failure/damage data of Table I and is listed by missile, component and category of failure. Due to the varied sources of data, it was not possible to make a quantitative assessment of the failures/damage, but it is apparent that the majority of failures were due to overstress during captive flight and handling.

To obtain a quantitative set or data on structural failures/damage to missiles the Fleet Analysis Center (FLTAC) at Corona Annex, Naval

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Failure
Structural
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TABLE

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	Ref.	25	21	ន	SI .	10, 15	<b>S</b>	<b>3</b> 2	-	<b>-</b>	-	-	<b>.</b>
	Comments	Three incidents reported 1971 thru 1974	Probable cause fin flutter (excessive moment @ joint)	9	Two incidents reported 1971-1974	One (1) incident reported 1971-1974	Separation occurred on arrested landing. Two (2) incidents 1971-1974	Pt. Magu fix	Fault detected after captive flight	Crack detected after cap- tive flight	8	4	<b>8</b>
	Fix	Lock on fins during captive flight	•	:	•	•	Lock fine dur- ing captive flight	Improved	Lock fin control surfaces during captive	Lock fin (canard) con- trol surfaces during captive filgi.	8	3	3
	Cause	Overstress	•	•	Rainstorm during flight	Hendling	Excessive load on joint	Lavironsent	Flight load overstress	Might load over- stress	4	4	**************************************
20 000	Tailure/Defect	Broke in 2 pieces after launch	Loose acrevs	G & C unit separated	Denged in flight	Denged	Warhead amparated from missile	Corresion of caper	Unequal gap between coupling ring & compo- ment	Creck	8	<b>8</b>	
Companient	Description	Missile	6 & C securing screus	G & C unit front joint attach serves	De se	Dom	Estherd Joint	Rolleron caper	Joine	Joint motor tube coupling ring groove	GCC compling ring grooves	TDD coupling ring grooves	Warhead coupling Ring grooves
	Missile	AIN-93 (Sidevinder)	3	3	3	\$	4	4	ADF-9C/0	8	*	4	\$

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Missile	Component Descristion	Type of	Couse	74.8	Commence	133
O/JAMIV	toupling ring screws	Correston, wrong acrev, or loose acrev	•	:	Detected after captive	~
4	Rolleron cager	Broken detent	Mendling	:	Detected during imspection	-
4	Wing assemblies	Correston	Leaky containers	Container		•
8	Bearing seals (rolleron)	Missing spony	Loss of epery Q.A.	Seal design	Detected during mainte-	•
4	Clamp ring CCC	Iroka	Tight load over-	Lock fin con- trol surfaces during captive	Crack detected after cap- tive flight	~
3	Snap ring, which holds outer bearing on relieven in place	Snap ring & bearing seal broken during vibration & shock testing	Design fault	New snap ring	Detected during flact use qualification testing	<b>.</b>
4	Wings	Correston	Inadequate packaging (packaged in wooden boxes)	Package in leak proof con-	Corroded during shipping & storage	=
AZN-90	Nolleron caging device	Shearing of rolleron caging device	Absence of caging clips during cap- tive flight	Proper instal- tion of caging clips	Caging clips loosened 6 lost during captive flight	2, 3
3	Hose come covers	Covers become loose after handling	Poor design	None	Loss of covers increases potential of damage to GOG and dome during handling	2
8	Dose.	Proken	Improper headling	•	Broken ducing shipping/	•
3	Varbeed	Broke off missile	Flight load over- stress	Lock on fin control sur- faces during captive fiight	Broke off during arrested landing	s.
\$	Rollstva demper	Damper leaking oil	Q.C. or hendling	Q.A.	Defect found during check- out of wing sesembly	п

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Missile	Cor, ment Description	Type of Failure/Defect	Cause	Pix	Comments	ığ
ADE-90	Dome.	Demagned in flight	Rafins torm	•	Six (6) incidents reported 1971-1974	2
1	Polleros cager detent	Cager detent broken	•	Material change	•	21
3	Missile	Water danage	Leaky container	Improve con- tainer design 6 inspection	Several incidents reported	<b>3</b>
4	Umbilical breakaney screws	Umbilical hang-up	Helicoile for screve inserted poorly	Q.A. insert helicoils properly	Launching problem. Launch delay caused	*
4DF-98	•	Crack in GCG lene	Handling	•	Crack noticed during tone-	=
ADS-92	•	Broken	Handling .	•	Broken during burn-in at Pt. Mugu	3
\$	Rolleron caging	Breakage of locking part of rolleron caging as- sembly which is plastic	Improper handling	Hone	Failures during handling	1
A18-9	Rolleron wheal	Wheel shifted on hus causing scuffing inside wall of case assembly	Lossened wheel on hub due to high centrifugal forces-no vases in front of rol- leron Air Force missile	Install flow vanes used on Mavy missiles 6 tighten force fit tolerances wheel/hub	Failures occurred during wind tunnel & flight tests	
ADI-70 (SPARIOV)	Ning.	Wing lost during captive	Overstress due to flutterving un- locked	:		ສ
AIN-70 AIN-71 AIN-712	Wing orac	Ving cities & wing stude broken loss of wings	Flutter insta- bility wings flap againt stops causing over- stress on stude	Wing clips to hold wings stationary dur- ing captive flight	Intermittent incidents date back to early 60's. Occurred on 74s Aftersit. Fallure could not be repeated when monitored during flight	*

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	Component Description	Type of Pailure/Defect	Cause	Plx	Coments	Bef.
×	Missile	Broke in two after firing	Overstress	•	Overciress probably caused by wing flutter (reference listed cause unknown)	2
	Pitch ving	Wing separated from	Flutter	•	Pitch wing separated after launch	2
	Laione & antenna	Partie	Foreign object in	•	2 occurrences during cap- tive filght1 foreign object and 2nd unknown cause	SI .
,	Ving mery.	7-5-6-7	Turbulence/wing instability	•	Eleven (II) assy's reported damaged after captive flight 1971 thru 1974	2
	Ladona	Demnged/shattered radoms	Hendling	•	3 occurrences 1971-1974. Dropped missile during	ង
_	U 4 9	G & C designed	Poor packs,ing	:	Damaged in container	21
	Varhead Mt 35/0	Veld defects	Manufacturing poor Q.C.	Q.A.	18 occurrences of weld defects 71-74	ង
	Aft verhead joint	weld failed	•	Add 47 rivets at joint		21
	Aft verhead joint	Insufficient number of rivets	Q.C. inspection	Improve Q.A.	Only 43 rivets found at joint where 47 called for	*
	Af entenna cornector	Broken	Improper handling	:	Broken during shipping/	~
	Ving shaft bearing	Corroston	Moisture intra-	Materproof bearing seals or acd anti- corrosive coat- ing to bearing	195 incidents F7 1972. Processed at MARF (Naval Air Revork Facilities)	a
	Demper assembly	isaking-failed specified test	Q.C. and captive flight environ- ment	Improve Q.A.	7.82 failure rate Jan thru March 1972, Reduced to 2.12 failure rate for FY 72.	a

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Typ Fedlur	Type of Failure/Defect	Cause	Fix	Comments	ref.
Demaged		Sendling	Maniling pro-	High rate of denoge reported IY-72	11
Loss of wing		Nutter	Material change to fiberglass	Material not necessarily cause of flutterfix questionable	2
Denaged		Handling	•	Six (6) sets reported dema_ed 1971-1974	n
Leskage at joint	ofac	Poor teflon coating	Tighter inspec- tion 6 call out on o-ring draw- ing	Tighter imagection 6 call out on o-ring draw-ing	•
Paraged		Handling	•	Demaged during storage unloading and loading handling (3 incidents, July thru Sept. 1974)	9

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TABLE 2. Failure/Damage--Grouped by Cause.

Cause of Failure/Damage	Missile	Components
Corrosion	AIM-9B	Rolleron cager
	AIM-9C/D .	Wings
	AIM-9G & ACM-45A	Various Components
	AGM-45A	Wing shaft bearing
	AIM-9C/D	Coupling ring screws
Handling	AGM-45	Umbilical cables
	AIM-9, AIM-7, AGM-45	Domes, radomes
	AIM-12B	RF antenna
	AGM-62	Wing/fin assy.
Quality control/	AIM-9	Bearing seals
quality	AIM-9	Rolleron damper assy.
assurance	AIM-9	Umbilical breakaway screws assy.
	AIM-7 & AIM-12B	Weld defects
	CHAPARRAL	0-ring
Captive flight	AIM-9. AIM-7	Domes
environment	AIM-9	Coupling rings, joints, screws
	AIM-9	Rolleron cager, rolleron snap ring, hub-rolleron
	AGM-45	Damper assy.
	AIM-7	Wing studs, clips, wings
	AGM-62	Wing

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TABLE 3. Summary of Failure/Damage Data By Missile.

Missile	Component	Cause & Type of Failure/Damage
AIM-9	Dome	Handling & captive flight environment (rain)Damage
	Joints	Captive flight overstress-cracks and breaking
	Rolleron caging assembly	Quality control and captive flight environmentbearing seals, dampers, snap ring, caging device.
	Wings	Corrosion
	Fins	Captive flightflutter creating overstress condition on missile joints
AIM-7	Radome & antenna	Handling and captive flight damage.
(SPARROW)	Wing assy.	Captive flight overstress wing studs and clips broken, loss of wings during captive and free flight.
AGM-45 (SHRIKE)	Wing damper assy.	Quality control and captive flight environmentfailed specified test, leaking after flight.
	Wing shaft bearings	Corrosion
	Umbilical cables	Handling damage
AGM-62	Wing/fin assy.	Handlingdamage
(WALLEYE)	Wings-aluminum	Ca tive flightflutter
AIM-12 (BULLPUP)	Aft warhead joint	Quality control mfgwelded joint failure.
(= 3=== ;	R.F. antenna connector	Handlingdamage

Weapons Station, Seal Beach, was requested to provide a summary of the physical defects and number of occurrences reported via Shore Maintenance Data Collection System (SMDCS) inspection reports for a period of 3 years (CY '73 - CY '75) for several missiles. Table IV shows the FLTAC data. The data do not indicate the cause of failures, but the type of defects/failures indicate that the majority occurred during handling and captive flight. The wing hub or lock damage reported on the AIM-7 (SPARROW) missile is due to the captive flight environment since it is of the same type shown in Table I.

Although corrosion is listed often in Table IV, the number of occurrences is insignificant when compared to those that are apparently due to handling or captive flight.

The summary of defects/failures presented in Table IV counts each report of a given physical defect, therefore, any defect reported more than once from separate inspections at separate locations for the same occurrence of that defect would result in multiple counts. For this reason, the number of occurrences reported in Table IV cannot be compared with any reports that deal with the <u>frequency of occurrence</u> of a given defect versus the number of times a given defect is <u>reported</u>.

Previous experience by FLTAC indicates that this discrepancy (a defect on the same missile reported more than once) should be less than 5% of the numbers (defects) reported in Table IV.

Table V provides data that allows the data of Table IV to be evaluated in relation to the total number of inspections reported during the three year time period covered, the number of go inspections (inspections with no defects), the number of defects reported that have no physical damage significance, etc.

Specific types of failure/damage are shown as a percentage of number of inspections in Table VI. Only the top nine failure/damage percentages are shown. The SPARROW (AIM-7) wing hub or lock damage exceeds the next type of damage reported by a factor of 5.

There are a number of dramatic statistics that can be obtained from the data shown in Table IV and V. For instance, taking a particular type of defect reported as a percentage of NOGO records with defects shows that the SPARROW wing hub or lock damage accounts for 33% of damage reported on the SPARROW. Similarly, 19% or approximately 1 of every 5 defects reported on the SHRIKE missile are radome damage. Damaged domes or radomes account for 4.6% of all defects reported for the missiles in Table IV.

Requirements for air launched missiles dictate that missile protuberances, such as control surfaces, be removable and packaged separately for logistical purposes (ease of packaging, storage and handling).

TABLE 4. Air Launch Missile Physical Defect Reporting Summary 1 January 1973 through 31 December 1975.

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AIM-54 (PHOENIX)

	• • • • • • • • • • • • • • • • • • • •	DEFECTS	
SECTION	<u> </u>	CODE	DESCRIPTION
ARMAMENT	m	ACP	CONNECTOR(S) PIN(S) BENT/DAMAGED (SPECIFY WHICH
	72	ACR	EXCESSIVE CORROSION OTHER DAMAGE
	10 21	ATA	OTHER DEFECT OR MISSING ITEM TDD ANTENNAS, ANY DAMAGE
CABLE	m	CAD	CABLE DAMAGE
CONTROL	~	CBD	ELECTRICAL POWER SUPPLY BATTERY ASSY DAMAGED
	<b>~</b>	933	CONNECTOR(S) DAMAGED
	25	000	REAR ANTENNA RADOME DAMAGE, OTHER
	<b>-</b>	۵ ن ن	CONFECTOR(S) PIN(S) BENT/DAMAGED (SPECIFY WHICH
	m	CCR	CONNECTOR(S) IN MARRATIVE) EXCESSIVE CORROSION
	<b>6</b>	000	OTHER DAMAGE
	~	CDR	DROPPED
	29	£	HYDRAULIC FLUID LEAK
	93	CHD	HYDRAULIC POWER SUPPLY FLUID LEVEL LOW
	 pung	CPO	ELECTRICAL POWER SUPPLY ELECTROLYTE EXIT PORT
	~	CRC	REAR ANTENNA BANDME CHT
	-	200	ELECTRICAL UMBILICAL DAMAGED
	~	COL	COOLANT UMBILICAL CONNECTOR LEAKING
	~	CXX	EXTERNAL MAINTENANCE REQUIRED
Z.	-9	F C C C	EXCESSIVE CORROSION
	}	•	
GUI DANCE	Φ.	000	
	<b>3</b> ~	9 C	RADOME CRACKED
	•		

TABLE 4. (Contd.)
AIM-54 (PHOENIX)

1

	-	DEFECTS	S
SECTION	<u>YI</u>	CODE	DESCRIPTION
PHOENIX ALL	m	WC W	COMPONENT/PART MISSING
UP ROUND	-	MCR	EXCESSIVE CORROSION ON ALL SECTIONS
•	15	MDO	OTHER DAMAGE
•		MOR	MISSILE DROPPED
	64	MFA	FUSELAGE INSULATION CUTS
	17	MF8	SECTION LAP JOINT BOLTS, ANY MISSING
	77	MFD	FUSELAGE INSULATION, DENTS/GOLGES
	18	MMO	OTHER DEFECT OR MISSING ITEM
	10	MSD	FUSELAGE METAL SKIN, DENTS/FLATS
	<b>د</b>	MUS	ELECTRICAL UMBILICAL WORN GUIDE SPERVES
	<b>4</b>	MXM	EXTERNAL MAINTENANCE REQUIRED
PROPULSION	84	PAD	ABMING MECHANISM ANY DAMACE
•	∞	PCC	ROCKET MOTOR EXIT CONE CHIPPED
	7	DPO	OTHER DAMAGE (EXPLAIN IN REMARKS)
WING	<b>v</b> .	MPD	PANEL, DENTS
	<b>.</b> †	<b>₹</b>	PANEL DAMAGED, OTHER

# TABLE 4. (Contd.) AIM-9 (SIDEWINDER)

SECTION	<u>212</u>	CODE	DESCRIPTION
N. I.	180	FNC	CORRODED TO EXCESS
GUIDANCE	562	CBD	CRACKED OR BROKEN DOMË
CONTROL	10	<u>د</u> ن د د د د د د د د د د د د د د د د د د د	CRACKED OR BROKEN MIRROR
1000	<b>?</b> /?	ງ ກິດ ເ	DEFECTIVE FIN BOOTS OR GROMMETS
	<b>-</b> 4	0FC	DAMAGED FIGURG CONTACTS
	700	) () () ()	DAINT ARPASIONS SCRATCHER OF HETA! DITTING
	12	<b>F</b> 00	
	ŧ	GAP	STRIPPED GAS PLUG
	113	00 <b>0</b>	DAMAGED TOD ALIGNMENT SLOT OR TDD/TLM
	16	GCR	CORRODED TO EXCESS
	9	g-:B	FIN BRACKET DAMAGE
		GFZ	FUZE CABLE DAMAGED/DEFECTIVE
	17	020	TLM CABLE DAMAGED/DEFECTIVE (DESCRIBE IN NARRATIVE)
	~	G10 <b>D</b>	TOD CABLE DAMAGED/DEFECTIVE
	201	GWD	WATER INTRUSION, WATER SOAKED
	23	011	ILLEGIBLE IDENTIFICATION
	-	NLO	NITROGEN LOW
	10	I Wd	PIN MISSING
ROCKET MOTOR	19	RAG	FAILED ALIGNMENT GUAGE TEST
	675	RCB	CONTACT BUTTON ASSY DAMGAGE OR CORRODED
	12	RCD	CONTAINER DAMAGED
	16	RCR	COUPLING RING CORRODED
	13	RF8	FWD. BULKHEAD CORRODED
	19	RFD	FUZE CONTACT PLUMGER DAMAGE OR CORROSION
	~	RHA	FAILS HANGER ALIGNMENT CHECK
	110	RHO	NON-PROPULSIVE HEAD CLOSURE DAMAGE
		RHT	FAILED LAUNCHER HOUSER TEST
•	24	RIF.	RIF ASSY GASKET MISSING OR DAMAGED
	1107	R11	ILLEGIBLE IDENTIFICATION
	-	RIT	INTEGRITY TEST FAILURE
	& \$	RLO	LAUNCH HANGER NOT SECURE OR DAMAGED

TABLE 4. (Contd.)
AIM-9 (SIDEWINDER)

		RUST, ETC)	•	ETC.  CORRODED ETC  WEATHER  CODE E)
	DESCRIPTION	MOTOR DROPPED (EXPLAIN IN REMARKS) NOZZLE DAMAGED (RUSTED, CORRODED) NOZZLE WEATHER SEAL CRACKED OR PUNCTURED PHYSICAL DAMAGE (CORROSION, DENTS, CUTS, RUST, RUBBER SEAL DAMAGED OR MISSING THREAD DAMAGE (COUPLING RING DAMAGE)	ALIGNMENT KEY MISSING COLOR CODE BAND MISSING CONHECTOR PINS BROKEN OR BENT GASKET DAMAGED, LOOSE OR MISSING HERMETIC SEAL BROKEN ILLEGIBLE IDENTIFICATION PHYSICAL DAMAGE SHOCK ABSORBER DAMAGED, LOOSE OR MISSING WATER DAMAGE OR CORROSION	EXCESSIVE CORROSSION COUPLING RING GROOVE DAMAGED COMPONENT MISSING COUPLING RING MISSING, BROKEN, CORRODED, ETC. THREADS DAMAGED OR CORRODED HOUSING PHYSICALLY DAMAGED IDENTIFICATION ILLEGIABLE O-RING DAMAGED OR MISSING O-RING GROUVE DAMAGE OTHER PHYSICAL DAMAGE OTHER PHYSICAL DAMAGE OTHER PHYSICAL DAMAGE SCREW MISSING, BROKEN, BENT, CORRODED ETC RADOME (RF WINDOW) DAMAGE RUBBER INSERT LOOSE, MISSING OR DAMAGED SCREW MISSING, BROKEN, CORRODED OR DAMAGED SCREW MISSING, BROKEN, CORRODED OR DAMAGED WATER SOAKED, WATER DAMAGED OR EXPOSED TO WEATHER EXTERNAL MAINTENANCE REQUIRED (CONDITION CODE E)
DEFECTS	CODE	R R S S S S S S S S S S S S S S S S S S	SAK SCC SCD SHS SPD SSA	1CD 1CG 1CG 1DC 1DC 1DC 1CR 1RD 1RD 1RD 1RD
	gīž	72 22 2991 38	333 333 333 450 83 83 83 83 83 83 83 83 83 83 83 83 83	2008 2018 272 272 66 66 66 73 84 84 84 84 84 84 84 84
	SECTION	RCCKET MOTOR (CON'T)	SAFE-ARM DEVICE	TARGET DETECTOR DEVICE

## TABLE 4. (Contd.) A14-9 (SIDEWINDER)

		DEFECTS	
SECTION	ğığ	CODE	DESCRIPTION
UMBILICAL CARIF	\$45	OCC	UMBILICAL CABLE COVERING PHYSICAL DAMAGE OTHER THAN
	167	UCD	SEPARATION FROM CONNECTOR SLEEVE UNBILICAL BLOCK CONNECTOR/CONNECTOR BENS MENT
	•	9	BROKEN, SHEARED, SHORTED, BURNED, OR MISSING
	•	9 0 0	UMBILICAL CONNECTOR BLOCK GASKET DEFECTIVE, LEAKING MISSING OF OTHER PHYSICAL DAMAGE
	9	CCA	UMBILICAL CABLE MISSING
	<b>~</b>	ncs	UMBILICAL CABLE COVERING SEPARATION FROM BLOCK
•	~	UCT	ECTION SLEEVE Lical cable fails TS-
	•		TEST
	۰,9	N C	UMBILICAL CABLE CORRODED, OR WEATHERED
		!	LINE BENT, BROKEH, OR SHEARED
•	1145	GPD	UMBILICAL PHYSICAL DAMAGE
	<b>8</b>	URP	UMBILICAL CABLE REPAIRED/REPLACED
	2514	OSA	UMBILICAL BLOCK CONNECTOR SCREWS DEFECTIVE, LODSE
			MISSING, DAMAGED, STRIPPED
WARHEAD	m	WCB	YELLOW BANK MISSING
	116	MCD	EXTROLOG CONTAINED DAMAGE
	549	MCO	HEAVY RUST OR CORPOSION ON MADDIEAR
	17	WCR	COUPLING RING DEFECTS
	v.	WO.	DAMAGED MATING ENDS
	^ !		EXPOSED EXPLOSIVE
	/61	IIA	ILLEGIBLE IDENTIFICATION (MARK, MOD, SERIAL NUMBER,
	56	MIS	LUI NUMBER) IMPROPER STORAGE OF WABHERS MOSETURE
	•		OF CONTAINER
	415	MPO	PHYSICALLY DAMAGED (DESCRIBE IN NARRATIVE)
÷	``	ASD	BULGES AT END OF SKIN, CRACKS OR HOLE IN SKIN
MING	94	MDO	PHYSICALLY DAMAGED, OTHER THAN AS LISTED HERE.
			(DESCRIBE IN NARRATIVE)

TABLE 4. (Contd.)

AIM-9 (SIDEWINDER)

CORRODED TO EXCESS CRACKS OF FLAWS DETECTED (X-RAY) DESCRIPTION DEFECTS CODE WNC WRC QIY WING (CON'T) 46 SECTION

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TABLE 4. (Contd.)
AIM-7 (SPARROW)

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		DEFECTS	
SECTION FEETION	<u>917</u>	CODE	DESCRIPTION
	37	AWCL	AWC-44 LOOSE
7		MHL	WING HUB OR LOCK DAMAGED
GROUP 1	165	YCA	MAGED OR
m	298	YCH	CHIMNEY, EPU, DAMAGED
	<b>5</b> ¢	YCM	T MISS
	36	VC0	CORROSION EXCESSIVE
	18	YCS	EPU CHIMNEY SEAL DAMAGED
	31	YCT	CABLE TUNNEL DAMAGE
	13	YEC	ELECTRICAL CONNECTION BAD
•	7	YEF	EPU FIRED
	206	YHO	WING HUB(S) DAMAGED
	<b>.</b>	YHL	HYDRAULIC OIL LEAK EXCESSIVE
••	210	XHX.	
		YMD	OR SECTION DROPPE
	35	YMO	MOISTURE INTRUSION
	30	YOT	OTHER
	18	YPB	PIN, BROKEN, SHORTED ETC.
51	978	YPD	CALLY DAMAGED (D
	209	YPL	
•4	210	YTC	TUNNEL COVER OR RELATED PARTS DAMAGED
	7	YUC	UMBILICAL CABLE DAMAGED
	Ś	YUP	AL PLUG DAM
	13	YWR	ASSY, REAR ANTENNA, D
	~	ZHM	, WIRING, DAMAGED OR
	m	ZWO	MOISTURE INTRUSION
RADOYE	83	XRD	RADONE DAMAGED
ROCKET MOTOR	11	RMI	MOISTURE INTRUSION
SPARROW ALL	m	ZMO	MOISTURE INTRUSION
TARGET SEEKER	4		THOOGH BOARD
	61	XCA XCA	CABLE DAMAGED OR BROKEN

19

TABLE 4. (Contd.)
AIM-7 (SPARROW)

SECTION Q TARGET SEEKER GROUP CONT'D)	911 6 100 8 200 8 200	91Y CODE DESCRIPTION 6 XCM COMPONENT/PART MISSING (DESCRIBE IN NARRATIVE) 8 ZCO CORROSION EXCESSIVE 1 ZMO MOISTURE INTRUSION
WARHEAD	11 WMI	MOISTURE INTRUSION, SUBMERGED, WATER SOAKED

## TABLE 4. (Contd.) ACM-45 (SHRIKE)

		DEFECTS	,
SECTION	ğıĭ	3000	DESCRIPTION
CONTROL	104	855	EXCESSIVE CORROSION
	975	ָר בּי	CONTROL CECTION BUNCTORY PRESENT THE STREET OF STREET
•	12	¥00	OA REJECT
	123	CSS	STRIPPED SCREWS, UNABLE TO REMOVE
	<b>&amp;</b>	900	•
	32	ΣÔ	UMBILICAL MISSING
	••	CUR	BROKEN PINS IN UMBILICAL RECEPTICLE
GUIDANCE	35	809	FXCFSSIVE CORPOSION
	116	04.5	GUIDANCE SECTION PHYSICAL DAMAGE
	œ <b>3</b>	<b>6</b> 0A	OA REJECT (REQUIRES EXTERNAL MAINTENANCE, CONDITION
		•	CODE E, ETC.)
	663	GRD	RADOME DAMAGE
	10	655	STRIPPED SCREWS, UNABLE TO REMOVE
	475	GTD	TOD ANTENNA DAMAGE
ROCKET MOTOR	67	MCD	AFT CLOSURE DAMAGE
	35	MCR.	EXCESSIVE CORROSION
	<u>*</u>	MDR	MUTOR DROPPED
	-	MFW	FRAYED MOTOR WIRE
	103	Σ Ω	IGHITER DEFECT
	65	a.	IGNITER OUT OF POSITION
	90	MPO	MOTOR SECTION PHYSICAL DAMAGE
	6. <del>1</del>	¥0.	QA REJECT
	_	MSS	STRIPPED SCREWS
SHRIKE ALL	25	RCM	MOISTUE IN CONTAINER
UP ROUND	23	RCR	CORROSION ON ALL SECTIONS
	ż.	ROR	ROULD DROPPED
WARHEAD	16	WCD	BAD WARHEAD CABLE
	32	¥CR	EXCESSIVE CORROSION
	~	XHX	FRAYED WIRE
	23	Odx	WARHEAD SECTION PHYSICAL DAMAGE

TABLE 4. (Contd.)

AGM-45 (SHRIKE)

'QA REJECT FUZE SAFE-ARM IN UNSAFE CONDITION DESCRIPTION DEFECTS CODE WQA <u>917</u> SECTION WARHEAD (CONT'D)

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TABLE 4. (Contd.)
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RIM-66, -67 (STANDARD ARM)

-		DEFECTS	S
SECTION	<u>YIY</u>	<b>200</b> 2	DESCRIPTION
AUTOPILOT BATTERY	19	APD	PHYSICAL DAMAGE PLUG MECHANICAL BAD (RECESSED PIN)
	<b></b>	AWD	
	± M	7 9 7 3 0 5	PHISICAL DAMAGE WATER DAMAGE OR CORROSION
	. <del></del>	PWS	
GUIDANCE	10	GRD	RADOME DAMAGE
	z	GRT	RADOME TIP LOOSE WATER DAMAGE OR CORROSION
CONANCE		OAD	ANTENNA DAMAGE
	· 60	000	DAMAGED MARK 20 CABLE
	200	OPD	
•	70	OMO	WATER DAMAGE OR CORROSION
OTHER	ĸ	BDA	BDA ANTENNA DAMAGED .
	45	MOM	DORSAL FINS DAMAGE
STEERING	1	SAC	ACTUATORS LEAKING FLUID
CONTROL	21	SPD	PHYSICAL DAMAGE
LIN		SPM	PLUG MECHANICAL BAD (PINS RECESSED)
	<u></u>	SSP	SHEARED TAIL RETAINING PIN
	ë o	STO SWD	TAILS OFF CENTER WATER DAGE OR CORROSION
STANDARD ARM ALL UP ROUND	11	MPD MVD	OTHER MISSILE PHYSICAL DAMAGE OTHER WATER DAMAGE OR CORROSION

TABLE 4. (Contd.)
AGM-62 (WALLEYE)

en.

DESCRIPTION	PHYSICALLY DAMAGED SMALL HOLE IN SECTION PUNCTURE HOLES IN SECTION FOREIGN MATTER PRESENT HARD POINT DECAL MISSING FILTER MOUNTING STUDS SHEARED	PHYSICALLY DAMAGED THREADS DAMAGED	RAT BLADE DAMAGED WATER IN SECTION PHYSICALLY DAMAGED HYDRAULIC OIL LEAKING RAT VIBRATION PRESENT RAT BLADES MISSING RAT SPLINE CRACKED	PHYSICALLY DAMAGED BOOSTER FROZEN PHYSICALLY DAMAGED	CAGER OPERATION FAILED MECHANICALLY PHYSICALLY DAMAGED	POTTING DAMAGED SERIAL NUMBER MISSING CONNECTOR DAMAGED CONNECTOR LOOSE IN MOLD ELECTRICALLY OPEN
CODE	APD APH AFM AMP	8PD 88T	CRD CWS CRC CRC CRC	FPD 28F 2PD	GCM	HPD HCD HCC HCC
\$IX	279 111 24 44 88	FUZE 4	99 K G G 4 K	# 11 m	431	<b>7</b> 8444
SECTION	ARMAMENT	BOOSTER,	CONTROL	FILTER FUZE	GUIDANCE	HARNESS

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TABLE

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EYE
ALL
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		DEFECT	DEFECTS
SECTION	<u>917</u>	CODE	DESCRIPTION
PROBE	7	PPD	PHYSICALLY DAMAGED
TRIGGER	m	TPD	PHYSICALLY DAMAGED

TABLE 5. Air Launch Missile Inspection Report Summary 1973 Through 31 December 1975.

Numb er	AIM-54 (PHOENIX)	AIH-9 (SIDEWINDER)	AIM-7 (SPARROW)	AGM-45 (SHRIKE)	RIM-66, -67 (STANDARD ARM)	AGY-62 (WALLEYE)
Inspection Records Processed GO Result Records NOGO Result Records NOGO Records w/o Defect Code NOGO Records w/Defect Code	5817 4247 1570 69 1501	86288 62579 23703 5597 18112	9658 3429 6229 388 5841	21285 17294 3991 469 3522	3520 2397 1123 126 997	7793 5586 2207 1116 1091
Defects Reported:						
Physical Defects Functional Defects Overage Pyrotechnics Other* Total	580 799 169 1548	20504 26 26 1188 518 22236	5562 327 1364 79 7332	3251 453 141 3845	295 414 413 42 1164	519 573 109 

\* "Other" category includes:
Gas Grain Expended
Invalid Defect Code Reported
Defects reported "other"
Modification required
X Ray required

TABLE 6. Failure/Damage—Relative to Number of Inspections for Different Types of Damage.

Missile	Description of Damage and component	Missile Section	7 Damaged (num- ber reported dam- aged + number of inspection rec- ords processed)
AIM-7 (SPARROW)	Overstress damage to wing hub or lock	Flight control group	20.1
AIM-9 (SIDEWINDER)	Handling damage to umbilical	Umbilical	4.2
AGM-62 (WALLEYE)	Handling physical damage	Armament section	3.6
AIM-9	Corrosion & handling damage such as dents and cuts to rocket motor	Rocket motor	<b>3.</b> 5
AGM-45 (SHRIKE)	Handling damage to radome	Guidance	3.1
AIM-9	Rubber insert loose, missing or damaged in target detecting device (TDD)	Target detecting device (TDD)	2.9
AIM-9	Excessive corrosion	Target detecting device (TDD)	2.3
AIM-54 (PHOENIX)	Dents, gouges & cuts in fuselage insula- tion/handling	Fuselage	2,2
RIM-66, -67 (STANDARD ARM)	Handling damage to ordnance	Ordnance	1.5

There have been and are many problems, as shown by the failure/damage data, associated with removable (mostly quick-disconnect) control surfaces. Every missile has had (or has) an instability, vibration, or flutter problem, which required costly analysis and fixes in an attempt to eliminate structural failures/damage. Typical examples of control surface caused failures are the: AIM-9 (SIDEWINDER) joint failures, due to overstress caused by wing flutter, which requires wing locks during captive flight and the AIM-7E (SPARROW) which has an ongoing problem, as shown by the number of wing studs and lock damage, although locks are used to prevent flutter. The locks used on the SPARROW wings are probably insufficient to prevent vibration caused by the free play due to tolerance build-up at the quick disconnect joint of the wing to shaft. Recently, the AIM-7F (SPARROW), with a different wing-to-shaft joint than the -7E model, has required design changes to resolve a flutter problem during free-flight. The AGM-45 (SHRIKE) missile had costly dampers added to the control section to prevent flutter of the quick disconnect wings during captive flight. Another problem with removable components has been water intrusion and corrosion at the mating joints of the parts.

The number of damaged domes and umbilical connectors during handling indicates that the protection used is inadequate or has a reverse effect on handling care, i.e., since a cover should protect a component from damage, it can therefore be subjected to rough and careless handling with the protection provided.

Table VII shows the number of physical defects as a percentage of inspections for each missile. The SPARROW missile had the highest percentage of defects (37.1%), this does not include the 1,978 physical defects described in the Appendix. The Appendix is a discussion of pertinent background information regarding the structural physical damage data provided by FLTAC.

### CONCLUSIONS

Types of failure/damage vary with time period, missile, type of use and inspection stations reporting the failure/damage. This conclusion is illustrated by comparing data of Table I, which were predominantly reported during the 1967 through 1974 time period and data of Table IV which is for CY 1973 through 1975. The primary cause of structural failure/damage of Table I was on the AIM-9 (SIDEWINDER) missile joints, which eventually was shown to be due to overstress conditions resulting from dynamic excursion of the missile caused by fin flutter. This problem was resolved prior to the 3 year period (1973-1975) reported by FLTAC, which shows the major damage problem on the SIDEWINDER to be umbilical damage. Another example of the shift of type and cause of damage is the corrosion damage on the AGM-45 (SHRIKE) missile. For CY 1973-1975

TABLE 7. Proportion of Physical Defects Reported for Each Missile Relative to Number of Inspection Records Processed.

Missile	Inspection Records Processed	Physical Defects Reported	% (physical defects     inspection     records)
AIM-7 (SPARROW)	9658	3584*	37.1*
AIM-9 (SIDEWINDER)	86288	20504	23.8
AGM-45 (SHRIKE)	21285	3251	15.3
AIM-54 (PHOENIX)	5817	580	10.0
RIM-66, -67 (STANDARD ARM)	3520	295	8.4
AGM-62 (WALLEYE)	7793	519	6.7

 $<sup>\</sup>star$  Does not include the 1,978 reported physical defects described in the Appendix.

data reported by FLTAC (Table IV), corrosion damage accounts for less than 1% of the missiles inspected, whereas reference 11 shows 17% of the missiles with corrosion damage for FY 1972. A reason for this shifting of types and causes of damage is due to the emphasis placed on a problem area when it becomes acute.

An overall view of the data studied indicates that handling and overstress conditions (not accounted for in design) during captive flight are the two major causes of structural failure/damage on air launched missiles.

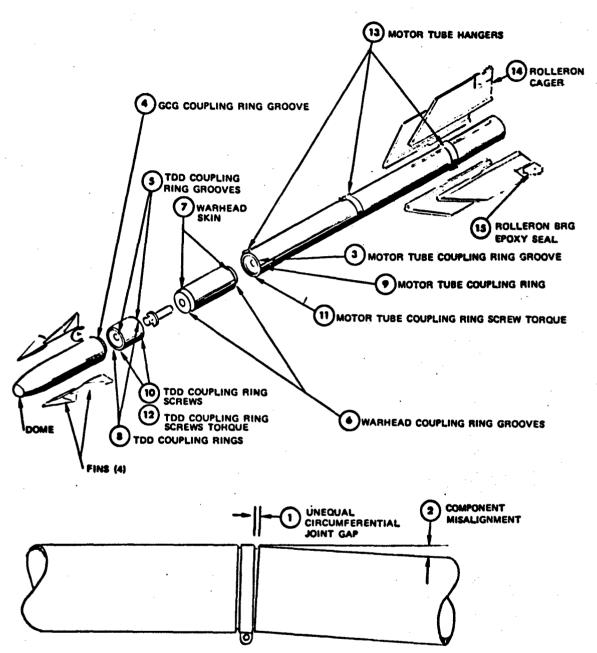
The majority of handling failure/damage appear to be caused by carelessness and inadequate protection of fragile parts of the missile during handling.

The majority of overstress conditions during flight have been caused by free floating, quick disconnect, moveable control surfaces, where the flutter or vibration of the surfaces causes high load conditions on attachment points and missile joints.

### RECOMMENDATIONS

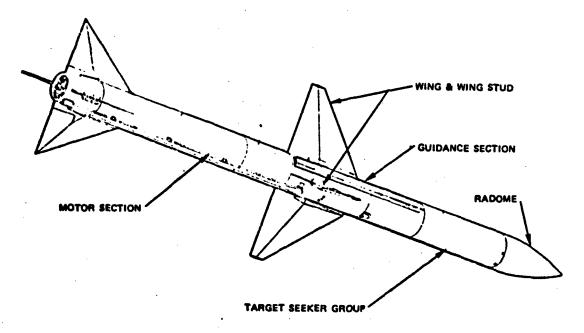
Since a majority of failures/damage occur during handling of missiles, it is recommended that a strong and ongoing program to eliminate negligence and carelessness be established. The program recently initiated by CONNAVAIRSYSCOM and the Fleet units (see Appendix) should be fully supported. It is also recommended that a review and investigation of the effectiveness of protective coverings on fragile missile components such as domes and umbilical connectors be initiated.

While there is no assurance that nonremovable control surfaces will not cause problems, the problems encountered with quick-disconnect removable surfaces (failures, damage and cost of fixes versus the logistics requirement) should be investigated. Although corrosion problems, due to inadequate packaging, have subsided in the last few years, there still appears to be a need for improvement as some corrosion during shipping and storage is being reported.



TYPICAL DEFECTIVE COUPLING RING JOINT

FIGURE 1. AIM-9C/9D Missile Failure Points.



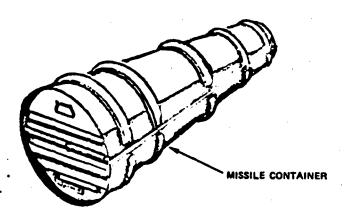


FIGURE 2. AIM-7 Missile Damage/Failure Points.

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### Appendix

### DISCUSSION OF PERTINENT BACKGROUND INFORMATION REGARDING ALM STRUCTURAL/PHYSICAL DAMAGE SUSCEPTIBILITY

- 1. It has been shown in the past that the vast majority of physical damage to Air Launch Missiles is detected on units returned to the Weapon Station from Fleet deployment. A program was recently implemented by COMNAVAIRSYSCOM and the Fleet units to bring about a reduction in this shipboard handling damage. This program has not yet been in force long enough for its effort to be reflected in current data. However, preliminary indications suggest that a noticeable reduction in damage resulting from negligent and careless missile handling will result.
- 2. In the following, a brief discussion of facts relevant to physical damage consideration for each of the six Air Launch Missiles addressed in this study is presented.

### a. PHOENIX (AIM-54)

The PHOENIX missile fuselage, except for the radome, is externally insulated with sheet cork bonded in place with a film adhesive and covered with nylon sheet (NOMEX). The function of this insulation is to provide heat protection for the missile components. By its nature, this insulation is susceptible to tears, scrapes, etc., and it is this damage which comprised approximately 25 percent of the PHOENIX Physical Defect codes considered in this study.

### b. SIDEWINDER (AIM-9)

A report of an earlier study included a discussion of SIDEWINDER visual inspection failure rates for the time period 1972-1974. The sample analyzed consisted of 7721 visual inspections conducted during the reporting period. These 7721 inspections represent the last inspection of a given GCG during a particular year. Results of these inspections were used to calculate GCG visual failure rates. The visual failure rate represents the proportion of the sample GCGs that were sent to NAVAIREWORKFAC solely on the basis of a visual inspection without a follow-on functional test because heavy physical damage prevented testing on the AN/DSM-78. The overall Visual Inspection Failure Rate was 0.13 (1042/7721). The distribution of defects for the 1042 rejected

GCGs showed that the three most frequent defect categories (cracked domes, umbilical screws, and skin damage) account for 61% of the total number of defects.

### c. SPARROW (AIM-7)

The 1978 "Physical Damage" defects listed for the Flight Control Group was used for some time to report "AWC-44 Loose" defects until a unique code was created for that defect. AWC-44 (Air Launch Weapon Change -44) added an assortment of gaskets, grommets and pressure pads in the cable tunnel and cable connector areas to preclude water intrusion into the section. During visual inspection, the integrity of the adhesive bond between the inside surface of the shell and the gasket added at the umbilical connector is evaluated. Improper priming of the metal surface prior to application of the bonding agent can and does result in an improper bond in this area and the resultant "AWC-44 Locse" defect code being reported. This defect is readily corrected at the Weapons Static Ithout the need to send the unit to the DOP for repair, and it does not represent a significant susceptibility to the unit to physical damage.

This is not the case, however, with the "Wing Hub or Lock Damaged" defect which was the most frequently reported serious physical defect for the SPARROW missile.

### d. SHRIKE (AGM-45)

The 975 CPD (Control Section Physical Damage) defects reported in enclosure (1) is inflated considerably by the presence of a considerable number (in excess of 500) of cases where that code was used, in the absence of a unique code for the purpose, to report screening and repair/replacement of the Barometric Pressure Switch in the control section. The remainder of the BPD defect codes covered a wide range of miscellaneous defects with no single defect prominent.

An earlier FLTAC study addressed the SHIRKE High Failure/Replacement Items from repair/rework data. The following is a synopsis of that study as it relates to physical damage.

### (1) Guidance Section

An evaluation of the data revealed the following items were major contributors to the SHRIKE guidance section repair at NARF during the reporting period 1969-1973: 511 TDD antennas replaced and 359 radomes replaced. Brief descriptions of the test results, replacement rates, and the reasons for the replacement of each item follows:

### TDD Antennas

A categorization of the reasons the antennas were replaced revealed that 418 were replaced due to physical damage and corrosion; 61 were missing upon receipt of the guidance section at NARF; 16 failed an electrical test; and the reasons for the replacement of the remaining 16 antennas were undetermined. There was a total of 706 guidance sections repaired and 511 antennas replaced for an average replacement rate of 0.72 (511/706). This means that slightly less than one antenna is replaced per guidance section repaired.

### Radomes

The primary reason for the replacement of 348 radomes was due to physical damage and corrosion which accounted for 97% of all radomes replaced. The remaining 11 guidance sections which required radome replacement had missing radomes when the guidance sections were received at NARF. The radome replacement rate for guidance sections repaired at NARF is determined to be 50.8% (359/706).

### (2) Control Section

The subassemblies and parts with the highest number of replacements at NARF for SHRIKE control sections resulting from physical damage during the period 1969-1973 were wing shaft bearings and umbilical cable assemblies.

### Wing Shaft Bearings

A total of 285 wing shaft bearings were replaced, corrosion being the sole reason. The cause of corrosion is probably salt water intrusion during Fleet deployment. At this time it is not known to what extent these corroded wing shaft bearings affect missile reliability or performance.

### Umbilical Cable Assemblies

A total of 169 umbilical cable assemblies were replaced: 83 were replaced for physical damage and/or corrosion; 76 were missing; and the remaining 10 failed an electrical continuity test. The umbilical cable is a frequently handled item during onloading and downloading operations aboard an aircraft carrier which may explain the high percentage.

### c. STANDARD ARM (RIM-66, -67)

There is no background information pertinent to the subject of Physical Damage available for the STANDARD ARM.

### e. WALLEYE (AGM-62)

The Ram Air Turbine (RAT) blade damage (including missing blades) continues to represent the most significant form of physical damage to the WALLEYE other than scratches, dents, and other external damage categorized "Physical Damage." An earlier study showed that RAT blade damage accounted for over 61 percent of the RATs replaced or repaired at the DOP.